

SYSTEM AND METHOD FOR REMOTELY DETECTING AND LOCATING DAMAGED CONDUCTORS IN A POWER SYSTEM

FIELD OF THE INVENTION

5 The present invention relates generally to power system maintenance and, more particularly, to a system and method for remotely detecting and locating damaged conductors in a power system.

BACKGROUND OF THE INVENTION

10 In many industries today, such as the avionics and automotive industries, complex and costly electrical components, systems and subsystems, as well as the electrical power systems powering these components, are interconnected by many bundles of conductors, typically wires, with each bundle including a plurality of wires. Although each wire is typically surrounded by insulation, or sheathing, such
15 wires can become faulty. In this regard, as the wires age, the insulation can breakdown and chaff. In such instances, the wires can contact other wires or other conductive structures, such as framework. Also, strands in aging wires can begin to separate and tear due to vibration, shock and stress on the wires. Stress due to pinching, rubbing, moisture, corrosion, excessive heat and/or lightening strikes also
20 pose risks that can lead to wire damage. Further, tight fitting connection points within connectors can loosen over time when subjected to the same environmental conditions as the conductors, and when subjected to numerous connects and disconnects due to replacement and maintenance of the electrical components, systems, subsystems, and the electrical power systems.

25 As will be appreciated by those skilled in the art, when the insulation surrounding the wires breaks down or chaffs, or the wire otherwise becomes faulty, undesirable electric arcs or other wire breakdown can occur at one or more locations along the wires, which can lead to breaks or shorts in the system. It will also be appreciated that in many instances, the location of such arc events or other wire

breakdowns can be difficult to find. In this regard, the location of an arc event or other wire breakdown may be inside of a bulkhead or inside of a wire bundle. Also, an arc event may only brown an area of occurrence without actually burning through or burning the insulation away from the affected wire.

5 In many instances, detecting and locating the arc event or other wire breakdown can be difficult, if not impossible. In this regard, detecting a fault in the system as being caused by a faulty wire may be difficult in systems that also include complex electrical components, systems, subsystems and power systems. As such, misdiagnosing a fault in the system as being caused by costly electrical components,
10 for example, can result in unnecessary replacement of such components while still failing to correct the fault.

In addition to the difficulty in detecting an arc event or other wire breakdown, locating such an arc event or other breakdown is also difficult. In many instances, the location of the arc event or other breakdown may be in a location that is impossible to
15 visually locate without extracting a wire bundle from the system. However, inspection of many feet of wire within a system can be very time consuming, and in some cases, may place maintenance personnel at risk for injury. Also, most conventional wire testing equipment is cumbersome and requires unique training of maintenance personnel as to how to use the equipment. Use of such equipment also
20 requires that one or more wire bundles be disconnected in order to test the wires. Unnecessary removal of equipment can also be very costly and time consuming, however, and can add to the required time to perform maintenance on the system. Further, many times such connection points are not located in easily accessed locations.

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SUMMARY OF THE INVENTION

In light of the foregoing background, the present invention provides a system and method of remotely detecting and locating damaged conductors. The system and method of embodiments of the present invention are capable of preventing
30 interference to loads during operation by conducting a test on a “dead conductor” before applying power to the load. By pre-testing the wire/load before power is applied, it is possible to prevent power from being applied to a damaged wire/load and may avert an arc event from occurring. The system and method of embodiments of the present invention may further provide the location of damage in a conductor,

such as the location of a suspected arc event. By locating the suspected damage, maintenance personnel may advantageously narrow the search for the damage to a specific location, even internal to a wiring bundle, without having to spend countless hours visually inspecting every wire from one end to the other.

5 According to one aspect of the present invention, a system is provided for remotely detecting and locating damaged conductors. The system includes at least one slave controller disposed proximate at least one load and electrically connected to the loads via at least one conductor. The slave controller includes at least one solid-state switch capable of controllably altering the input current to the loads, as well as at
10 least one measuring element for measuring at least one parameter, such as at least one current parameter, associated with the loads and the solid-state switches. In this regard, the solid-state switch can controllably alter the input current to the loads according to the parameters. Advantageously, the system also includes at least one damaged wire detector electrically connected to the conductors between the slave
15 controller and the loads. The damaged wire detector is capable of detecting and/or locating at least one damaged conductor. Each damaged wire detector can also be capable of notifying a respective slave controller when the damaged wire detector detects a damaged conductor such that the at least one solid-state switch of the respective slave controller can alter the input current to the at least one load.

20 More particularly, the solid-state switches can operate in an on mode wherein the solid-state switches permit a respective load to receive the input current, and/or an off mode wherein the solid-state switches prevent the respective load from receiving the input current. When the solid-state switches operate in the off mode, the damaged wire detectors are capable of testing the conductors to thereby detect and/or locate at
25 least one damaged conductor before the solid-state switches are placed in the on mode.

 The damaged wire detectors can detect and/or locate a damaged conductor in a number of different manners. For example, each damaged wire detector can be capable of detecting and/or locating at least one damaged conductor by transmitting at
30 least one test pulse along at least one respective conductor and receiving at least one reflection from the respective conductors. Thereafter, the respective damaged wire detector can compare the reflections to reference data to thereby detect and/or locate at least one damaged conductor. The damaged wire detector can be further capable of

converting the reflected signal into digital data representative of the reflections that are then compared to reference data, such as previously stored reference data.

Each damaged wire detector can be further capable of determining at least one length of the conductors based upon at least one transit time between transmission of the test pulses and reception of the respective reflections. In such instances, each damaged wire detector can be capable of comparing the reflections to reference data by comparing the determined lengths to at least one reference length. In this regard, comparing the determined lengths to the reference lengths can include detecting at least one damaged conductor when the determined lengths are shorter than the respective reference lengths by more than a threshold length. Also, each damaged wire detector can be capable of locating the damage as a point on the respective conductors at the determined lengths.

According to another aspect of the present invention, a method of remotely detecting and locating damaged conductors is also provided. Therefore, embodiments of the present invention provide a system and method for remotely detecting and locating damaged conductors. Embodiments of the present invention allow for non-intrusive testing of the power cables, which reduces wear and tear on cable connectors and keeps maintenance personnel from having to enter cramped quarters to conduct tests. This reduces the potential of secondary damage due to wiring being disturbed by personnel crawling on the wires. Being able to test wiring from external locations can reduce unnecessary vehicle or structure entry and reduce the potential for incidental damage. Cable inspection times can also be reduced due to automated processes and being able to conduct tests from external to system locations.

BRIEF DESCRIPTION OF THE DRAWINGS

Having thus described the invention in general terms, reference will now be made to the accompanying drawings, which are not necessarily drawn to scale, and wherein:

FIG. 1 is a block diagram of a system of remotely controlling at least one load according to one embodiment of the present invention;

FIG. 2 is a block diagram of a damaged wire detector according to one embodiment of the present invention;

FIG. 3 is a block diagram of a programmable controller including a single solid-state switch and multiple measuring devices according to one embodiment;

provide either alternating current (AC) current and voltage or direct current (DC) current and voltage to the loads, depending upon operation of the loads. As shown and described herein, however, the programmable controller is particularly adapted to provide DC current and voltage to the loads. But it should be understood that the
5 programmable controller can equally provide AC current and voltage to one or more loads, as desired.

The programmable controller **10** can be electrically connected to the loads **14** via electrical conductors, such as copper wires or the like. By using one programmable controller to control multiple loads, and by disposing the controller
10 proximate the loads as opposed to in one central, humanly accessible location, cabling in the system is reduced which, in turn, reduces parasitic impedance in the system, and reduces the weight of the system. The programmable controller can be electrically connected to a remote master controller **12**, such as a high-level processor or computer, which controls the input current to the loads through the programmable
15 controller. Although the programmable controller can be electrically connected to the master controller, the programmable controller can additionally, or alternatively, be configured to operate independent of the master controller or any other type of controller.

Electrically connected between the programmable controller **10** and the loads
20 **14**, the system includes a damaged wire detector **16**. The damaged wire detector is capable of monitoring the impedance conditions associated with the conductors connecting the programmable controller to the loads, as well as the loads **14**. Typically, the conductors are tested before applying power to the loads to thereby prevent malfunction in the system upon applying power to the loads. The damaged
25 wire detector can detect a damaged wire and locate the damage in any of a number of different manners, such as according to a time domain reflectometry technique, as described below.

The programmable controller **10** and the remote master controller **12** can each draw power from a variety of sources as such are known to those skilled in the art.
30 For example, in devices such as airplanes and automobiles, the programmable controller and remote master controller, in addition to the loads **14**, can draw power from the device's existing power bus. Additionally, or alternatively, the programmable controller and/or master controller can be connected to a stand-alone power source that supplies power to the programmable controller and/or master

controller. The master controller of the system can additionally be connected to various other electrical systems within various devices. For example, in the automotive industry, the master controller can interface with the vehicle management system and carry out the vehicle management system instructions to the loads in an autonomous fashion. It should be understood that, although the system illustrated depicts one programmable controller electrically connected to one master controller, a single master controller can be, and preferably is, electrically connected to multiple remote programmable controllers without departing from the spirit and scope of the present invention. In turn, a damaged wire detector **16** can be, and preferably is, electrically connected between each programmable controller and the loads connected to the respective programmable controller.

As previously mentioned, the master controller **12** controls the input current to the loads **14** through the programmable controller **10**. As such, the programmable controller can be used as a power relay or a circuit breaker, depending upon the desired application and the types of loads connected. As discussed below with reference to the programmable controller controlling the loads, the master controller controls the programmable controller by continuously monitoring the programmable controller, controlling the output current from the programmable controller to the loads such as in on and off modes, selecting the various system parameters such as current, voltage and temperature limits, and programming the various system parameters into the programmable controller. Alternatively, or additionally, the programmable controller can be preprogrammed before integration into a device and run free from control from the master controller. Therefore, throughout the description of the present invention, reference will only be made to the programmable controller. But it should be understood that the control features of the programmable controller can be performed by the master controller and/or the programmable controller. For more information on such a programmable controller, see U.S. Patent Application No. 09/842,967, entitled: *Programmable Controller For Remotely Controlling Input Power Through a Switch to a Load and an Associated Method of Operation*, filed April 26, 2001, the contents of which are hereby incorporated by reference in its entirety.

Reference is now drawn to FIG. 2, which illustrates a schematic block diagram of a damaged wire detector **16** according to one embodiment of the present invention. The damaged wire detector includes a processing element **18** capable of controlling

operation of a time domain reflectometry (TDR) module **20**. As described more fully below, the processing element can be capable of transmitting signals onto the conductors between the programmable controller **10** and the loads **14**, and receiving digital data representative of signals reflected back from the conductors. In this
5 regard, the damaged wire detector can include an oscillator **21** capable of driving the processing element to transmit signals and receive the digital data.

In addition to the processing element and oscillator **21**, the damaged wire detector can include an isolation transformer **22** capable of injecting a pulse onto the output. The TDR module is capable of transmitting a series of test pulses down the
10 conductors connecting the programmable controller **10** and the loads **14**. Each test pulse can propagate down the conductors and, at a termination point, reflect back to the TDR module, which can receive the reflection and thereafter generate digital data representative of the reflection. Thereafter, the processing element **18** can analyze the digital data to determine if a conductor is damaged and attempt to identify a location
15 of the damage.

More particularly, the TDR module **20** can comprise a driver **24** through which each test pulse is driven onto the conductors via the isolation transformer **22**. The test pulse can comprise any of a number of different predetermined pulses, such as a 1 microsecond, 5 volt analog pulse. In this regard, the test pulses can be
20 comprise 1 MHz test pulses, which provides 10 nano-second resolution, or on the order of one to two meter distance resolution for typical conductors. If desired, the test pulse can be passed through a resistor **25**, such as a 25 Ohm resistor, before passing through the transformer to thereby give the driver an output impedance that forms a driver with the conductor impedance. Upon receiving the reflection back
25 from the conductors via the transformer, the analog reflection can be converted to digital data representative of the reflection by passing through a comparator **26**, which compares the analog reflection to an analog pulse width modulated (PWM) controlled DC threshold signal, as such will be appreciated by those skilled in the art.

To allow the TDR module **20** to receive reflections of different magnitudes to
30 thereby detect termination points of different magnitudes and at different lengths along the conductors, the reflection from each test pulse can be converted to digital data with different thresholds. For example, the reflections can be converted to digital data with different thresholds by comparing the reflections to a DC threshold level reference generated from an adjustable PWM signal. In this regard, the magnitude of

the threshold signal, and thus the threshold of the resulting digital data, can be set by a level adjust element **28**. Also, before passing through the level adjust element, the threshold signal can be filtered, such as by filter **30**, which can comprise any of a number of different conventional electrical elements, such as resistors **30a**, capacitors **30b** or the like. In this regard, the threshold signal can be filtered to generate the DC threshold level reference. The DC threshold level reference can then be scaled and offset to produce threshold level settings for the comparator **26**. The threshold level settings can comprise any of a number of different levels, but in one embodiment, the threshold signals range from +7 volts to -7 volts in approximately 0.78 volt increments.

After converting the analog reflections to digital data representative of the reflections, the digital data can be passed to the processing element **18** for analysis to determine if a conductor is damaged and attempt to identify a location of the damage. The digital data can be passed to the processing element in any of a number of different manners, such as by being passed directly to the processing element. In a more typical embodiment, however, the digital data is passed to a buffer, such as a first-in-first-out (FIFO) buffer **32**, which thereafter passes the digital data to the processing element. The FIFO buffer can comprise any of a number of known FIFO buffers, such as a 512 x 1 FIFO buffer. The FIFO buffer permits the processing element **18** to control the TDR module **20** to generate test pulses at a frequency of 1 MHz (i.e., 1 microsecond test pulses), while receiving the digital data at a lower rate. Operation of the FIFO can be controlled by an oscillator **34** that, in turn, is controlled by the processing element. In this regard, receipt by the processing element of the digital data can be controlled by controlling the oscillator. As such, the processing element can enable operation of the TDR module **20** via control of the oscillator.

The oscillator **34** can clock the digital data into the FIFO buffer **32** from the comparator **26** at any of a number of different rates such as, for example, at 100 MHz. Similarly, the oscillator can clock the digital data from the FIFO buffer to the processing element **18** at any of a number of different rates, such as at 100 MHz. In addition to passing the digital data to the processing element, the FIFO buffer can also output the clock signal from the oscillator **34** to the processing element. In this regard, the processing element can receive the digital data and associated clock signals such that the processing element can synchronize the digital data with reference data for comparison to determine if the conductors are damaged.

More particularly, the processing element **18** can compare the digital data with reference data in memory to determine if the conductors are damaged. As will be appreciated by those skilled in the art, according to the time domain reflectometry technique, as the test pulses are transmitted down the conductors, all or part of the pulse energy is reflected back along the conductors when the pulses reach the end of the conductor or reach a location that has been damaged along the length of the conductor. The processing element can then measure the transit time required for each test pulse to travel down the conductors and reflect back, and convert the time to distance, which is thereafter compared to a reference length. The reference length can be determined in any number of different manners, such as from the reference data. The reference data, in turn, can comprise data stored in memory, such as during "calibration" of the TDR module **20**. As will be appreciated, distances determined from the digital data that are significantly shorter than corresponding distances determined from the reference data can be regarded as locations of damage along the length of the conductors. The differences between the distances determined from the digital data and the corresponding distances determined from the reference data required to indicate a location of damage can be selected in any of a number of different manners to provide any of a number of different levels of tolerance of the system. For example, the difference required to indicate the location of damage can be selected to be greater than five percent of the distance determined from the reference data.

The processing element **18** is capable of communicating with the programmable controller **10**. In this regard, the programmable controller can clock data into and out of the processing element, such as distances determined from the digital data and/or the reference data, utilizing signal lines TDR CLOCK and TDR DATA as shown in FIG. 2. In addition, the processing element can transmit a notification, alert or the like to the programmable controller, such as when the differences between the distances determined from the digital data and the corresponding distances determined from the reference data required to indicate a location of damage exceed a threshold, as described more fully below. As shown in FIG. 2, then, such a notification, alert or the like can be transmitted to the programmable controller utilizing the FAULT ALERT signal line.

Referring now to FIG. 3, the programmable controller **10** of one embodiment of the present invention includes a controller processing element **36**. The controller

processing element can be any of a variety of processors, such as, for example, the PIC17C752 microcontroller manufactured by Microchip Technology Inc. The controller processing element monitors and controls the functions of at least one, and preferably multiple, solid-state switches 40, discussed below. Not only does the
5 controller processing element monitor and control the functions of the switches, the controller processing element also determines a condition of the switches and/or loads by performing calculations in the firmware using preconfigured characteristics and measured parameters of the switches and/or loads. The controller processing element allows the programmable controller to provide flexibility to the power system of the
10 present invention not available with conventional circuit breakers or relays. By emulating the material limitations of conventional circuit breakers and relays with firmware, the controller processing element of the programmable controller overcomes the material limitations of conventional circuit breakers and relays, by having the capability to reprogram the controller processing element for different
15 loads, as opposed to changing discrete components (i.e., conventional circuit breakers and relays). Also, the programmable controller allows for a wide variety of power control implementations to be programmed and made selectable by the system, such as various trip-curve implementations. In addition, the controller processing element can caution an operator if a dangerous condition is encountered, or the controller
20 processing element can automatically control the respective switch accordingly.

The programmable controller 10 also includes at least one, and preferably more than one, solid-state switch 40, each connected to a respective load 14. While the illustration of FIG. 3 depicts only a single solid-state switch, it should be understood that the figure is for illustrative purposes only, and should not be taken to
25 limit the scope of the present invention. In one embodiment, illustrated in FIG. 4, each solid-state switch includes a switching element 49, a drive element 48 and a switch-protection element 46. While the switching element can comprise any number of different solid-state switches, such as a MOSFET or an IGBT, the switching element acts to alter the input current to the respective load, typically operating in
30 either an on mode wherein the switching element permits the respective load to receive the input current, or an off mode wherein the switching element prevents the respective load from receiving the input current. As previously stated, a solid-state switch eliminates the mechanical contacts of conventional circuit breakers and relays

which, in turn, reduces the erosion and other problems associated with mechanical contacts.

The solid-state switch **40** also includes a drive element **48** that provides the input current to the switching element **49**, and typically comprises circuitry consisting of conventional electrical components such as resistors, diodes and transistors. Additionally, the solid-state switch may include a switch-protection element **46** that protects the switching element against instantaneous over-current conditions that could damage the switching element. The switch-protection element can comprise any of a number of different configurations, but, like the drive element, typically comprises conventional electrical components such as diodes, transistors, resistors and capacitors.

In operation, the switch-protection element **46** senses an actual current through the switching element **49**. If the actual current is above a predetermined value, such as a maximum current rating of the switching element, the switch-protection element alters the actual current through the switching element so that the actual current is no more than the predetermined value, typically placing the switching element in the off mode. In some instances when the solid-state switch **40** is initialized at start-up, an inrush of actual current flows through the switching element. But while this current may be above the predetermined value, it typically settles down to a level at or below the predetermined value within a fairly short time. To account for this inrush of current and prevent the switch-protection element from prematurely altering the input current, the switch-protection element of one embodiment is capable of waiting a predetermined amount of time before monitoring the level of current through the switching element. This predetermined amount of time allows the level of current to settle to a more constant, operation level before the switch-protection element monitors the switching element for instantaneous over-current situations. Additionally, or alternatively, the switch-protection element can be configured to control the actual current in different manners at different times or in different modes of operation. For example, the switch-protection element can be configured to step down the predetermined value at which current is interrupted from an initial, elevated value to a stable, constant value at the conclusion of the predetermined amount of time.

Referring again to FIG. 3, the programmable controller **10** of the present invention includes at least one, and preferably more than one, measuring element that

measures various conditions of the loads 14 and solid-state switches 40. For example, the programmable controller may include a current measuring element 38 and/or a voltage measuring element 42 that measure the input current through and voltage drop across a respective load. Additionally, the programmable controller may include a

5 temperature measuring element 44 that measures the temperature at or around the solid-state switch. The current and voltage measuring elements are typically made from conventional electrical components such as resistors, capacitors and operational amplifiers. Also, the temperature measuring device can be made from any number of devices, such as the LM75 digital temperature sensor, manufactured by National

10 Semiconductor. In operation, the measuring elements protect the loads 14 and/or solid-state switches 40 from undesirable conditions such as over-current, over and under voltage, and over and under temperature conditions by comparing such measured parameters against predetermined values for the respective load and/or switch. For example, the predetermined value for each load may be based upon

15 material characteristics of the load, such as a maximum current or voltage rating, or a minimum operational voltage. Also, for example, the predetermined temperature value for each solid-state switch may comprise a maximum temperature rating for the respective solid-state switch, over which damage is caused to the solid-state switch. Additionally, the predetermined value based upon current or voltage rating

20 characteristics can additionally take into account the predetermined temperature value because the current and voltage characteristics of various loads typically change over a range of temperatures.

Referring to FIG. 5, typically, the controller processing element 36 compares the measured parameters against the predetermined values by first constructing a

25 model trip curve 50 comprising a plurality of measured parameter values at different points in time. The controller processing element compares the model trip curve against a characteristic trip curve 52 for the respective load and/or switch. The characteristic trip curve is typically predefined based upon a characteristic of the switch and/or load associated with the particular parameter, such as a current rating

30 characteristic trip curve associated with the measured input current through the switch and/or to the load. FIG. 5 illustrates a characteristic trip curve along with a constructed model trip curve for a switch and/or a load with a ten amp current rating. Although not illustrated, the characteristic trip curve can additionally be predefined based upon a combination of the various parameters associated with the switch and/or

load, such as the temperature of the switch and/or load along with another parameter of the switch and/or load since many parameters of the switch and/or load may vary depending on the temperature of the switch and/or load. The characteristic trip curve is stored by the controller processing element or an associated memory device, thus making any trip curve implementation possible, such as I^2T and tiered. The predetermined values of the characteristic trip curve are defined to prevent the solid-state switch and/or load from operating too long in a dangerous area 56. By referencing the characteristic trip curve, the controller processing element can keep the measured parameter in a safe area 58, such as below the current rating of the switch and/or the load, and turn off the switch before the switch and/or load can be damaged by crossing a critical point 54 on the characteristic trip curve. If the condition measured by the respective measuring element falls outside the range of predetermined values or above the predetermined value or, more typically, if the model trip curve constructed by the controller processing element based upon the measured parameter or parameters is predicted to reach the critical point on the characteristic trip curve, the controller processing element alters the input current through the solid-state switch accordingly. For example, if the controller processing element in conjunction with the measuring element determine that the input current to the load will remain at or above a certain level for more than the maximum time permitted by the characteristic trip curve within a predefined period of time, the controller processing element can alter the input current to bring the measured value within the predetermined value range or below the predetermined value or, preferably, the controller processing element can place the solid-state switch in the on or off mode.

25 In another advantageous embodiment, when the input current to the switch and/or the load reaches or exceeds a certain level, such as a maximum current rating or an input current rating, respectively, the controller processing element repeatedly increases a count. If the count exceeds a predetermined threshold representative of the predefined period of time, the controller processing element can alter the input current to reduce the input current to below the certain level, such as by placing the switch in the off mode. But if the input current to the load decreases to below the certain level before the count exceeds the threshold, the controller processing element will repeatedly decrease the count. In this regard, the controller processing element can account for previous current stress (e.g., excess current) to the switch and/or the

load should the switch and/or the load experience a subsequent current stress before the count reaches zero since the count would begin upward again, although not from zero but from a value representative of the residual stress on the switch and/or the load.

5 Referring now to FIG. 6, a method of remotely controlling the input current from the controller processing element 36 through each switch 40 to each load 14, according to one embodiment of the present invention, begins by configuring the firmware of the controller processing element based upon the desired characteristics of the switches and loads, such as current and voltage ratings of each load, a
10 maximum current rating of each switch and/or a temperature rating of each switch, as shown in block 100. For example, the firmware can be configured with the characteristic trip curves typically predefined based upon the characteristics of the switch and/or load. Additionally, the characteristic trip curves can be predefined based upon a combination of the various characteristics of the switch and/or load,
15 such as the temperature of the switch and/or load along with another parameter of the switch and/or load since many parameters of the switch and/or load may vary depending on the temperature of the switch and/or load. Thus, different characteristic trip curves can be utilized depending upon the temperature of the switch. Additionally, or alternatively, the characteristics of each switch related to current
20 through the switch, such as the maximum current rating, can be configured into the respective switch-protection element 42 to monitor the actual current through the respective switch. Advantageously, by configuring the controller processing element with the characteristics of the switches and loads, if a switch or load with different characteristics is connected to the power system, the controller processing element
25 can be reconfigured such as by constructing and storing the characteristic trip curves associated with the different switch or load, as opposed to replacing the discrete components of conventional circuit breakers and relays.

After the controller processing element 36 has been configured, the damaged wire detector 16 can operate to determine whether any of the conductors are damaged
30 and, if so, determine the location of the damage. Referring now to FIG. 6B, a method of detecting and locating each damage in each conductor begins by transmitting a set of test pulses, such as a set of 1 microsecond, 5 volt analog pulses, down the conductors, as shown in block 122. The comparator 26 can then receive reflections of the test pulses, and thereafter compare the convert the analog reflections to digital

data representative of the reflections, as shown in block 124. In this regard, the comparator preferably compares the reflection of each test pulse to a threshold signal of a different magnitude, such as by comparing the test pulses to threshold signals ranging from +7 volts to -7 volts in approximately 0.78 volt increments.

5 The digital data representative of the reflections can then be compared to reference digital data to determine whether the digital data is within a threshold of the reference digital data. More particularly, the transit time required for each test pulse to travel down the conductors and reflect back can be determined from the digital data, which can thereafter be converted to a length. The length can then be compared
10 against a reference length determined from the reference digital data to thereby determine if the length determined from the digital data is lengthwise within a threshold of the reference length. In this regard, the reference digital data can be representative of reflections from known properly operating conductors of the same length and makeup as the conductors tested, as shown in block 126. The reference
15 digital data can be generated in any of a number of different manners but, in one embodiment described below, the reference digital data is generated by training the damaged wire detector 16 using the conductors at an instance in which it is known that the conductors are functioning properly, such as just after configuring the programmable controller 10 with the damaged wire detector and the loads 14. The
20 threshold can equally be set in any of a number of different manners. In one embodiment, for example, the threshold is set at five percent of the reference digital data (i.e., the distance determined from the digital data is within five percent of the distance determined from the reference digital data).

 During the comparison, if the digital data is within a threshold of the reference
25 digital data, the conductor is considered to be functioning properly without any damage. Thereafter, a determination is made as to whether all of the conductors have been tested for damage, as shown in block 130. If all of the conductors have not been tested, another conductor is selected, as shown in block 132. The process can then repeat for the next conductor, beginning with issuing the test pulses down the next
30 conductor, as shown in block 122.

 If the digital data is not within the threshold of the reference digital data, the processing element 18 can store the digital data and report the damaged conductor, such as to the programmable controller 10. In a more typical embodiment, however, if the digital data is not within the threshold of the reference digital data, the one or

more subsequent tests are performed on the same conductor to verify the damage to the conductor. In this regard, if the digital data is not within the threshold of the reference digital data, the processing element determines whether a predetermined number of passes (e.g., two) have been taken at the respective conductor, as shown in
5 block 134. In other terms, the processing element determines if the respective conductor has failed the test a predetermined number of times by failing to be within the threshold of the reference digital data during any such test. If the predetermined number of passes have not been taken, the process can repeat for the respective conductor, such as beginning with issuing the test pulses, as shown in block 122.

10 If the predetermined number of passes have been taken and damage has been detected with each pass, however, the processing element can store the digital data and report the damaged conductor (FAULT ALERT), as shown in block 136 and described more fully below. As will be appreciated, if the programmable controller receives notification that a conductor is damaged, such as by the digital data for the
15 respective conductor not being within the reference digital data after a predetermined number of passes, the programmable controller will typically prevent current from being applied to the respective conductor, as such is described above.

After testing the conductors with the damaged wire detector 16, and presuming the damaged wire detectors do not detect a damaged conductor, each
20 switch 40 is operated in the on mode, as desired, to provide the input current to the respective load 14, as shown in block 102. As the switch is operating in the on mode, the switch-protection element senses the actual current through the switch, as illustrated in block 104. If the actual current is above a predetermined value, such as the maximum current rating of the switch, the switch-protection element can wait a
25 predetermined amount of time to allow any inrush of current to settle to a stable level, as shown in blocks 106 and 108. Additionally, or alternatively, the switch-protection element can be configured to control the actual current at different times or in different modes of operation. For example, the switch-protection element and/or controller processing element can be configured to step down the predetermined value
30 from an initial, elevated value to a stable value at the conclusion of the predetermined amount of time. If, after the predetermined amount of time the actual current is still above the predetermined value, the switch-protection element reduces the actual current, such as by placing the switch in the off mode, as shown in blocks 111 and 120). In the event the actual current is below the predetermined value, either initially

or after the predetermined period of time, the switch-protection element continuously monitors the actual current to ensure the actual current remains below the predetermined value, as shown in blocks **110** and **111**.

5 As the switch-protection element **46** monitors the switch **40** for an over-current situation, the controller processing element **36** periodically samples the current and/or voltage through and/or across the load **14**, and/or samples the temperature of or around the switch to use to obtain a condition of the load and/or switch, as illustrated in block **112**. The condition is then determined by comparing the current, voltage and/or temperature against the characteristics predefined by the
10 controller processing element.

The controller processing element can determine if an over temperature or under temperature condition exists in the switch, as shown in block **114**. And if so, the controller processing element can alter the input current accordingly. For example, the temperature measuring element can measure the air temperature at or
15 around the switch and compare the measured temperature against the predetermined values for the desired temperature range, such as critical temperature limits. If the measured temperature is below or above the desired temperature range, the controller processing element can place the respective switch in the off mode to prevent the switch from being damaged or from damaging the respective load, as shown in block
20 **120**. Alternatively, the controller processing element can construct different characteristic trip curves based upon other parameters to emulate the temperature at or around the switch based upon characteristics of the switch that vary in proportion to the temperature of the switch.

The controller processing element can also determine if an over voltage or
25 under voltage condition exists in the load **14** and alter the input current accordingly, as shown in block **116**. For example, if the measured voltage drop across a respective load falls outside the preconfigured voltage range for the respective load, the controller processing element **36** can alter the input current to place the voltage drop within the desired levels or place the respective switch **40** in the off mode.

30 The controller processing element **36** can also determine if an over current condition exists in the load **14** and, if so, alter the input current to below the predetermined level, as shown in block **124**. For example, the controller processing element can determine a model trip curve **50** using a plurality of measured parameter values at different points in time. The controller processing element compares the

model trip curve against the characteristic trip curve **52** for the respective load and/or switch **40**. The predetermined values in the characteristic trip curve are defined to prevent the switch from operating too long in the dangerous area **56**. Additionally, the controller processing element can account for previous current stresses (e.g.,
5 previous switch operations in the dangerous area) by maintaining a count. As the switch operates in the dangerous area, the controller processing element repeatedly increases the count. And if the switch returns to operating outside of the dangerous area before the count reaches a predetermined threshold (representative of the maximum amount of time the switch is allowed to operate in the dangerous area), the
10 controller processing element can repeatedly decrease the count as long as the switch remains outside the dangerous area, as previously described. By referencing the characteristic trip curve, the controller processing element can turn off the switch before the switch and/or load can be damaged, such as by placing the switch in the off mode, as shown in block **120**.

15 As indicated above, the reference digital data can be generated in any of a number of different manners but, in one embodiment, the reference digital data is generated by training the damaged wire detector **16** using the conductors at an instance in which it is known that the conductors are functioning properly. In this regard, in one embodiment, before the conductors are tested, the damaged wire
20 detector can enter a maintenance mode whereby the conductors proceed through a training process to generate reference digital data that is thereafter stored for subsequent use during testing of the conductors. During training of the damaged wire detector, the processing element can transmit a set of test pulses down the conductors and receive reflections back from the conductors. The reflections can then be
25 converted into digital data representative of the reflections by passing the analog reflections through the comparator **26** with the reflection for each test pulse compared to a threshold signal of a different magnitude. The digital data can then pass through the FIFO **32** to the processing element **18**, which stores the digital data as reference digital data.

30 In addition to training, the damaged wire detector **16** can enter the maintenance mode to perform a number of other maintenance/troubleshooting functions of the system. For example, in instances in which the processing element **18** has stored digital data associated with a failed test, the damaged wire detector can enter maintenance mode to thereby extract and, if desired, further analyze the digital

data. The digital data can be extracted from the processing element in any of a number of different known manners by another processing device, such as a personal computer, laptop computer or other high level processor. Thereafter, if desired, the digital data can be further analyzed to determine the location of the damage in the
5 conductors.

In one embodiment, the digital data, as well as the reference digital data, can be presented on a display, such as by plotting each as a separate waveform. In this regard, FIG. 7 illustrates an example of digital data plotted against reference digital data for a conductor having a length of fifty feet terminated at a load. As shown, the
10 reference digital data (left plot) is compared against the digital data (right plot) acquired in accordance with embodiments of the present invention. As shown, the digital data (right plot) differs substantially from the reference digital data (left plot). Thus, the display of FIG. 7 may illustrate a damaged conductor. Further, as shown at the bottom of the display of FIG. 7, the length of the conductor is determined to equal
15 12.55 feet, which differs substantially from the actual length of the conductor, fifty feet. In contrast, in instances in which the conductor is not damaged, the reference digital data (left plot) is typically substantially similar to the digital data (right plot).

In another embodiment of the present invention, shown in FIG. 8, the system can further include an arc fault detector 70 electrically connected between the
20 programmable controller 10 and the loads 14. In this embodiment, the arc fault detector is capable of monitoring the current flow through the programmable controller for anomalies associated with an arc event. Then, when one or more such anomalies are identified by the arc fault detector, the arc fault detector can notify the programmable controller of the event so that the programmable controller can place
25 respective switches 40 in the off mode to prevent the respective load from being damaged by an arc event. For more information on such an arc fault detector 70, as well as the system including both the damaged wire detector 16 and the arc fault detector, see U.S. Patent Application No. _____, entitled: *System, Arc Fault Detector and Method for Remotely Detecting and Locating Arc Electric*
30 *Events in A Power System*, filed September 15, 2003; and U.S. Patent Application No. _____, entitled: *System, Supplemental Protection Module and Method for Remotely Detecting and Locating Faults in A Power System*, filed concurrently herewith, the contents of both of which are hereby incorporated by reference in their entirety.

Embodiments of the present invention therefore provide a system and method for remotely detecting and locating damaged conductors that allows for non-intrusive testing of the power cables. As such, wear and tear on cable connectors can be reduced, and maintenance personnel can be kept from having to enter cramped
5 quarters to conduct tests. By keeping personnel from having to enter cramped quarters, the potential of secondary damage can be reduced due to wiring being disturbed by personnel crawling on the wires. Being able to test wiring from external locations can also reduce unnecessary vehicle or structure entry and reduce the potential for incidental damage. Further, cable inspection times can be reduced due to
10 automated processes and being able to conduct test from external to system locations.

Many modifications and other embodiments of the invention will come to mind to one skilled in the art to which this invention pertains having the benefit of the teachings presented in the foregoing descriptions and the associated drawings. Therefore, it is to be understood that the invention is not to be limited to the specific
15 embodiments disclosed and that modifications and other embodiments are intended to be included within the scope of the appended claims. Although specific terms are employed herein, they are used in a generic and descriptive sense only and not for purposes of limitation.